Metering Dispensation

Caergeiliog – GT2

1 Background

As part of the Anglesey Distribution Network reinforcement scheme, SP Manweb have installed a 2nd 132/33kV Grid Transformer at Caergeiliog substation (GT2). This additional Grid Transformer helps to maintain supplies for the underlying Amlwch/Caergeiliog group on the isle of Anglesey.

The connection to supply GT2 from the National Grid network for this arrangement differs from typical supply arrangements elsewhere in the SP Manweb Network. The connection is ultimately derived from Wylfa GSP (with National Grid owning and operating the 132kV Busbars at Wylfa). The connection for Caergeiliog GT2 is via a teed connection to a National Grid 132kV owned circuit (EV Line) at tower location EV79 which runs from Wylfa to Penrhos and the south of the island. This Tee point location is some 18km from Wylfa.

A newly constructed SP Manweb 132kV circuit connects this "Interface" point to the SP Manweb Network via a 1.4km circuit into Caergeiliog and GT2 and then onto the 33kV busbars. This is illustrated below.

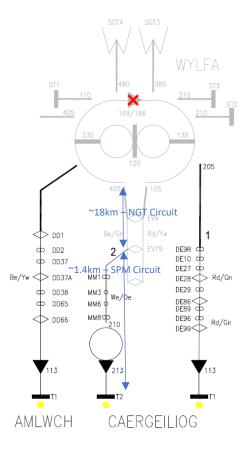


Figure 1 - Outline supply arrangement (Wylfa)

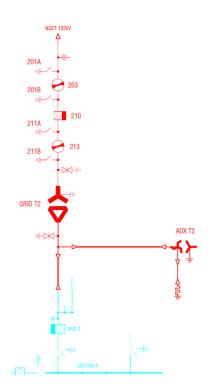


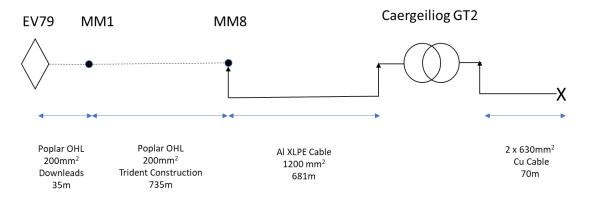
Figure 2 – Operational Diagram - (Caergeiliog GT2)

Due to the remote location and practicalities of locating a meter at the National Grid / SP Manweb interface point and tee off point on tower EV79, a dispensation is required as it is proposed the metered is located at Caergeiliog and at 33kV.

The losses therefore with the SPM network assets from the metering location at Caergeiliog GT2/33kV to the EV79 Tee off point at the 132kV interface needs to be taken into account as these would not be accounted for at the remote metering location as they would be upstream of the meters location and so not be visible.

<u>2 SLD</u>

The diagram below shows a single line diagram representation of the connection from the tower EV79 Tee off to Caergeiliog GT2/33kV.





3 Impedance data used

3.1 Conductors 132kV

The conductors used are standard supplied equipment. As such, their impedance, reactance and resistance values already exist with the SPM Manweb IPSA Power system model and conductor database. Further information on the installed span lengths are provided in Appendix A.

In summary the base impedance information for the 132kV circuits is illustrated below. Note that a typical modelling system base of 100MVA has been applied as unless otherwise stated.

Base Impedance		R1, pu per km	X1, pu per km	R0, pu per km	X0, pu per km	B, uS pu per km
200mm AAAC Poplar	OHL - Trident	0.0007461	0.002169	0.0015509	0.007504	0.000535
1200mm XLPE AL Cable	Cable - Ducteo	0.017219251	0.009090909	0.056684492	0.034224599	0.000143336
Circuit data used		R1, pu	V1	D0	¥0	DC. mark
circuit data used		KI, pu	X1, pu	R0, pu	X0, pu	B, uS pu
200mm AAAC Poplar	OHL - Trident	0.000574146		0.001193464		0.000411699
		0.000574146	0.001669111		0.005774553	

3.2 Conductors 33kV

The base impedance information for the 33kV circuit (GT2 Tails) is illustrated below.

Base Impedance	R1, pu per km	X1, pu per km	R0, pu per km	X0, pu per km	B, uS pu per km
1 x 630mm CU XLPE	0.003857	0.009231	0.01157	0.009231	0.001163
2 x 630mm CU XLPE	0.0019285	0.0046155	0.005785	0.0046155	0.002326
Circuit data used	R1, pu	X1, pu	R0, pu	X0, pu	B, uS pu
2 x 630mm CU XLPE	0.0001350	0.0003231	0.0004050	0.0003231	0.0001628

The IPSA model data tables are also provided in Appendix B for completeness and shows agreement with the data tables here.

3.3 Caergeiliog 132/33kV GT2

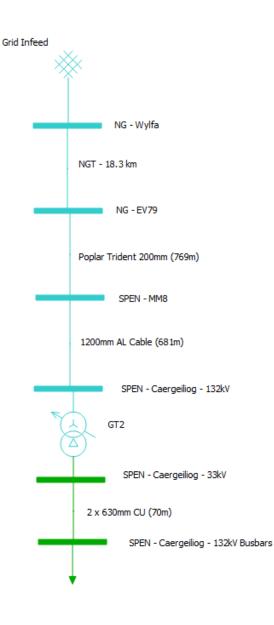
The actual Grid transformer name plate Impedance information is provided in Appendix C for completeness. SP Manweb has a standard 60MVA Grid transformer specification and impedance envelope (typically 20% impedance on rating). This is necessary to ensure system fault level infeed compliance and voltage regulation. Transformer X/R ratios of 25 and zero sequence to positive sequence impedance ratios of 85% are typical.

It is important to note that, in this instance, these values are solely for load flow purposes as the Grid Transformer losses are specified and shown in Appendix C on the nameplate. These losses are therefore taken into account in the calculations as they are based on the transformers FAT measurement results (Factory Acceptance Test) and so it is prudent to use these.

4 Modelling

4.1 IPSA V2 Model

An IPSA model was established to calculate the circuit losses. The values used in the IPSA model are shown in Appendix B, and are based on the data previously discussed. This data matches that within the SPM complete network model, but this simple model was created for simplicity. The model is illustrated below.





4.2 Losses - Circuit

Circuit losses were calculated using IPSA for a range of transformer loadings, up to the rating of the transformer at 60 MVA. This was done for unity power factor and a power factor of 0.95. The diagram below shows the losses for a transformer load factor of 0.3, 0.6 and 1, or 20, 40 and 60MVA.

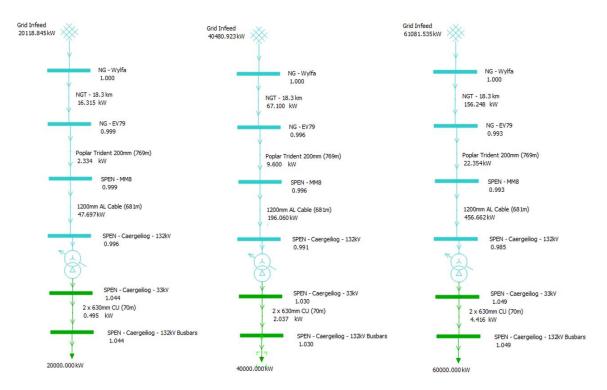


Figure 5 – IPSA Model example circuit losses for transformer load factor of 0.3, 0.6 & 1 at UPF

As mentioned before, we are only concerned with the losses from the NG – EV79 location to Caergeiliog. The losses therefore for the upstream National Grid line is illustrated but has been omitted from the summations. The values for the model for the National Grid EV line was provided to SPEN and is the same as that used within this and the SPEN whole system model.

Circuit ohmic losses are typically proportional to the square of the current, and this can be seen from above.

4.3 Losses - Transformer

As shown in Appendix C, the transformer name plate shows the losses within the 60MVA GT2 as P0=17.08kW and Pk=185.68kW. These have therefore been applied and again have been on a basis they are proportional to the square of the transformer load factor.

4.4 Losses - Adjustment

From the IPSA results, data outlined and shown in the Appendices, an adjustment curve can be derived and applied to the actual observed metered reading. This adjustment takes cognisance of the inferred upstream losses from the 33kV meter location to the EV79 POC as a result of SPM's:

- 1. 33kV Grid Transformer tails (2 x 630mm² CU Cable 70m)
- 2. 132/33kV Caergeiliog GT 2 (60MVA 20.27% on rating)
- 3. MM 132kV circuit from Caergeiliog to EV79 Tee location
 - a. Cable section (1200mm² AL Cable 681m)
 - b. OHL Trident section (200mm² Poplar OHL 735m)
 - c. Downleads (200mm² Poplar OHL –35m)

Note the Figure 6 and the proposed measured kW adjustment has an intercept of 17.08kW, as this takes into account the no load losses for Caergeiliog GT 2 as per nameplate.

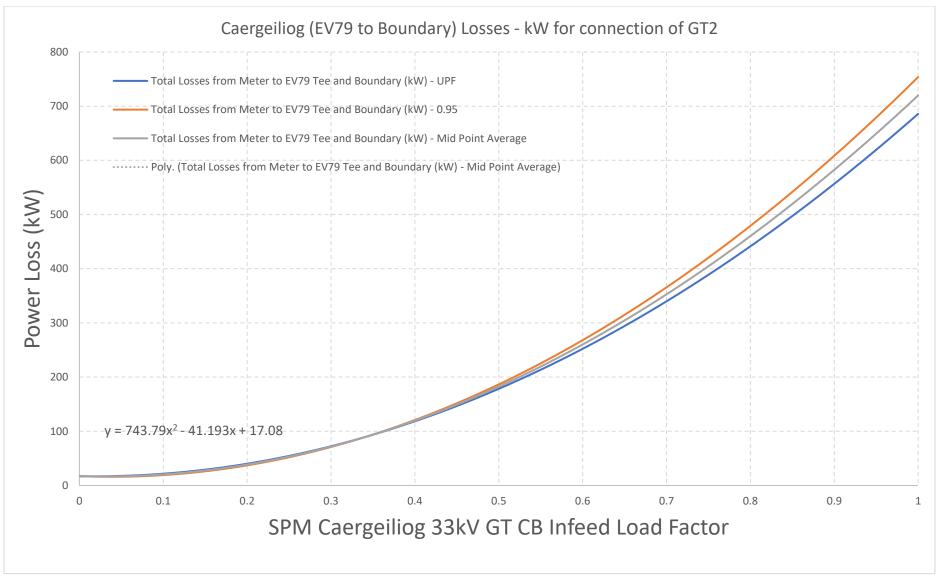


Figure 6 – Caergeiliog (EV79 to Boundary) Losses - kW for connection of GT2

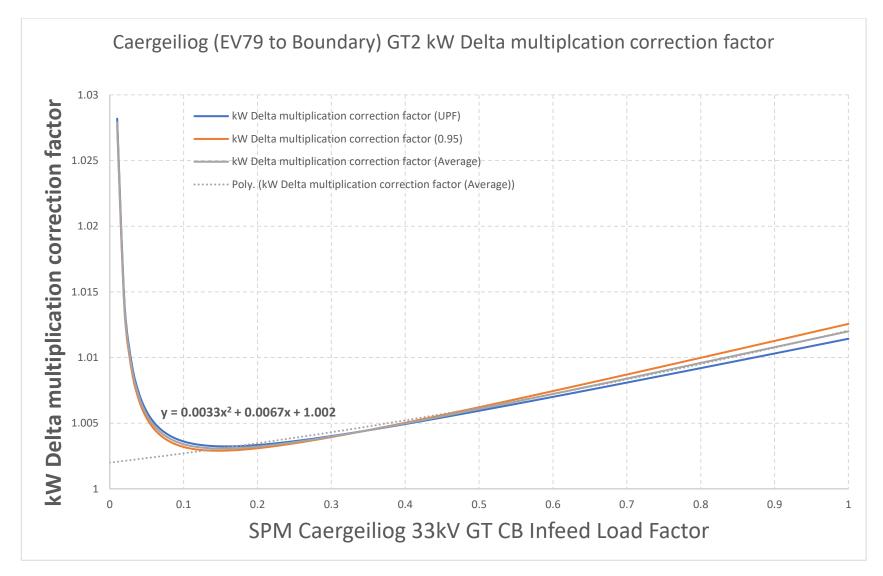
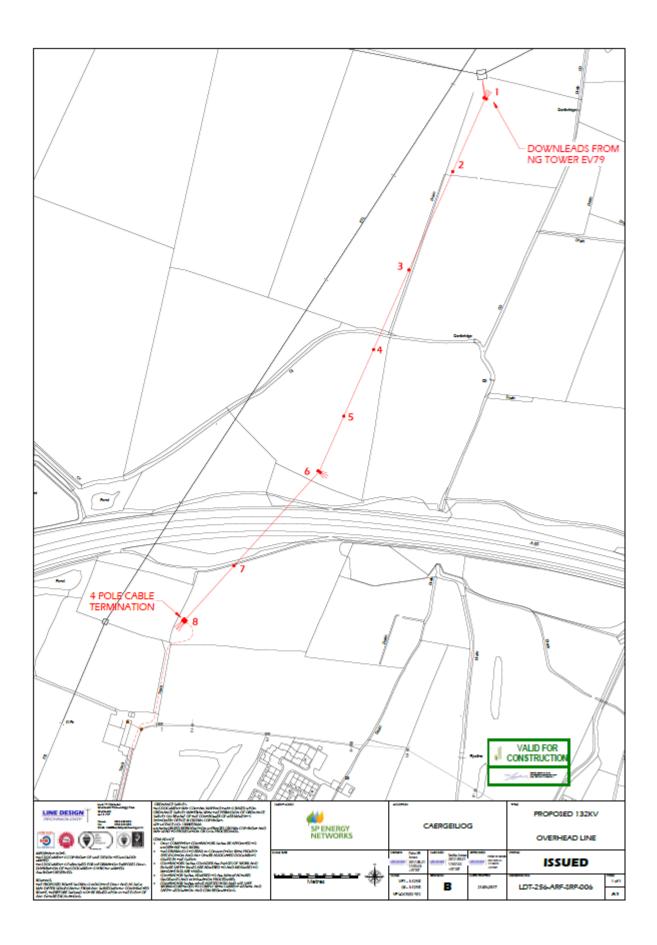


Figure 7 – Caergeiliog (EV79 to Boundary) Losses - kW for connection of GT2

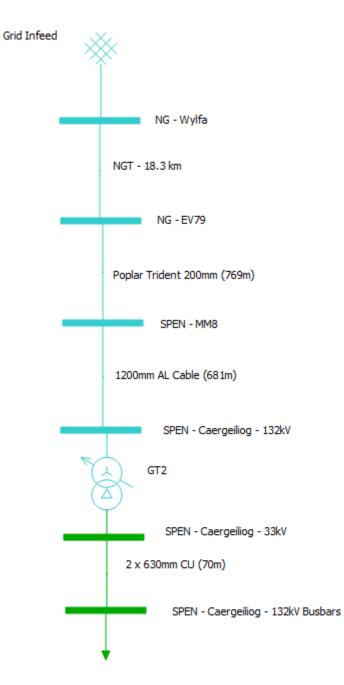
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m	INTER 2.5m ARM	E	365	3.00	L	129.67	,		m						435007	
4	INTER 2.5m ARM	15	385	2.75	L	104.65			m						435007	
2	INTER 2.5m ARM	m	365	2.75	u.	87.82			m						435007	
9	ANGLE H-POLE	12	320	2.00	2	73.09	491.63	18.IR		m	9	9	7/4.00	0	435010	Failure Containment Structure
2	INTER 2.5m ARM	12	385	2.75	т	152.76									435007	
8	TERMINAL H-POLE	15	370	2.00	2	90.14	242.9				m	4	7/4.00	E	435011	4 Pole Cable Terminal Structure
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Appendix A – EV79 Tee to Caergeiliog SPEN 132kV Circuit



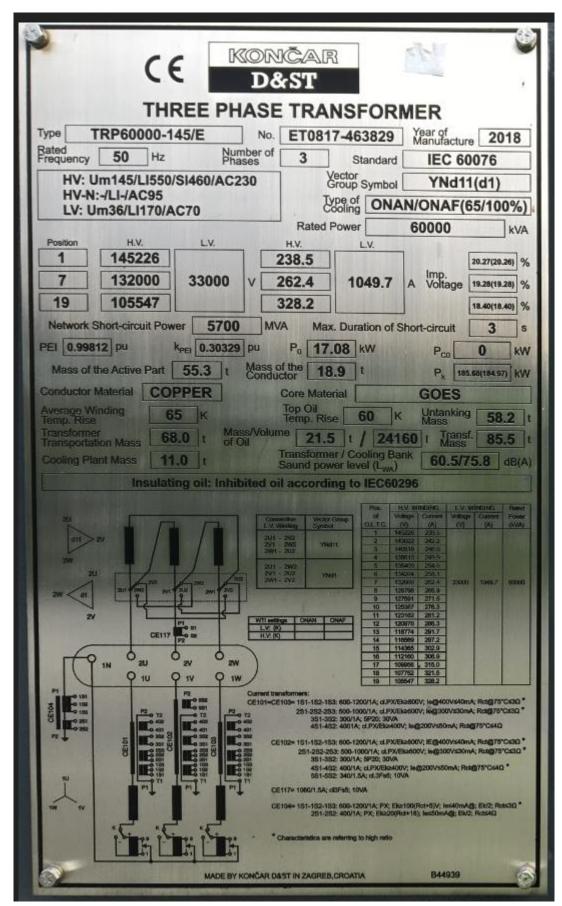
Appendix B – IPSA Model



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Pea	k LG (MVA)	9000	RMS	lg (MVA)	3500				
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Appendix C – Caergeiliog GT2 Namplate